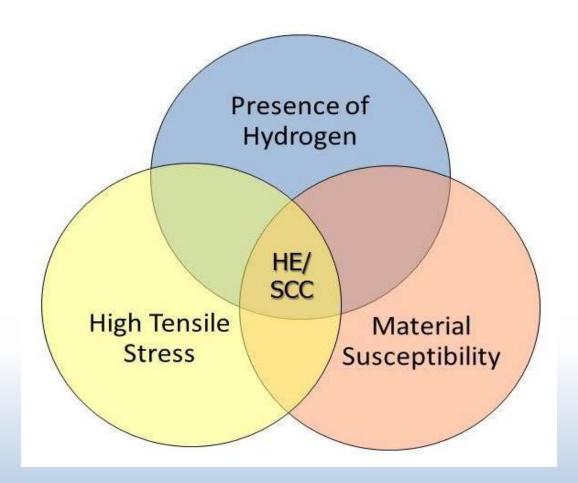
## Briefing on Bay Bridge Bolts – July 10, 2013



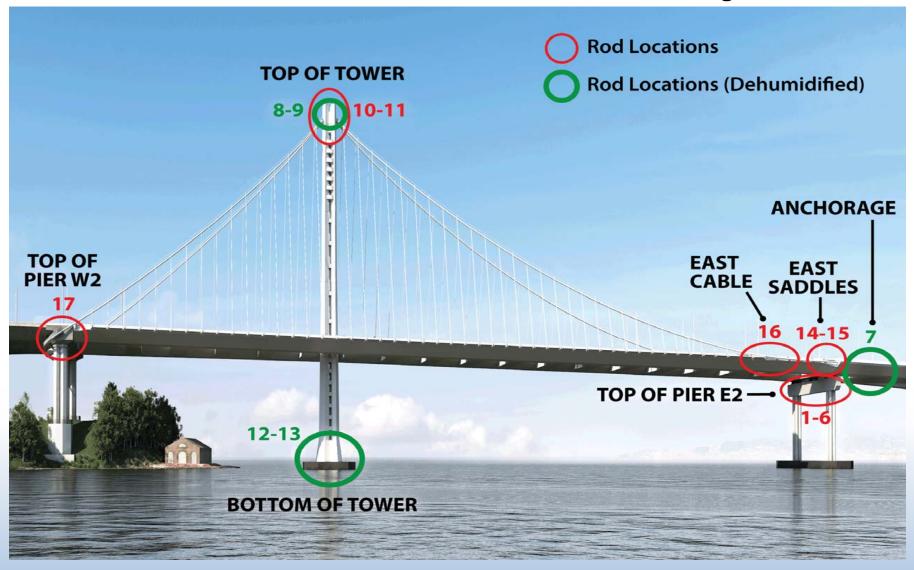
## Items Expected at July 10 BATA Briefing

- Completion of written TBPOC investigative report, <u>plus</u>
- Firm schedule for E2 2008 bolt retrofit, plus
- Decision on other bolts on SAS, equals
- Decision on Seismic Safety Opening Date of Bay Bridge.

## Causes of Hydrogen Embrittlement (HE) or Stress Corrosion Cracking (SCC)



#### A354 Grade BD Rod Locations on the SAS Bridge



#### A354 Grade BD Rods on the SAS Bridge

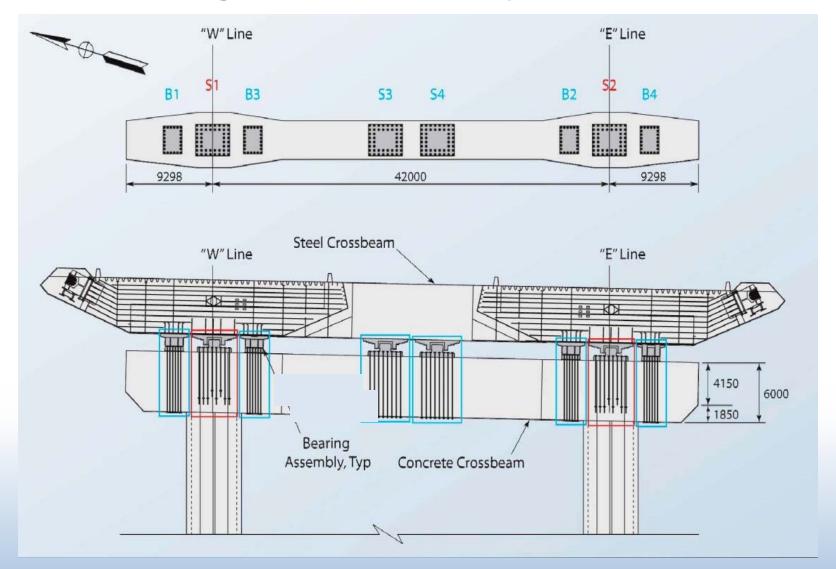
Item No.	Location	Component	Quantity Installed	Diameter (in)	Length (ft)	Tension (fraction of Fu*)
1		Shear Key Anchor Rods (2008)	96	3	10-17	0.7
2	Top of Pier E2	Bearing & Shear Key Anchor Rods	192	3	22-23	0.7
3		Shear Key Rods (top)	320	3	2-4.5	0.7
4		Bearing Rods (top)	224	2	4	0.7
5		Bearing Assembly	96	1	2.5	0.6
6		Bearing Retainer Ring Plate Assembly	336	1	0.2	0.4
7	Anchorage	Parallel Wire Strands (PWS) Anchor Rods	274	3.5	28-32	0.3
8	Top of Tower	Saddle Tie Rods	25	4	6-18	0.7
9		Saddle Turned Rods	108	3	1.5-2	0.5
10		Saddle Grillage	90	3	1	0.1
11		Outrigger Boom	4	3	2	0.1
12	Bottom of	Tower Anchor Rods (Type 1)	388	3	26	0.5
13	Tower	Tower Anchor Rods (Type 2)	36	4	26	0.4
14	East Saddles	East Saddle Anchor Rods	32	2	3	0.1
15		East Saddle Tie Rods	18	3	5	0.1
16	East Cable	Cable Band Anchor Rod	24	3	10-11	0.2
17	Top of Pier W2	Bikepath Anchor Rods	43	1.2	1.5	TBD
		TOTAL QUANTITY	2,306			



# **Looking Back**

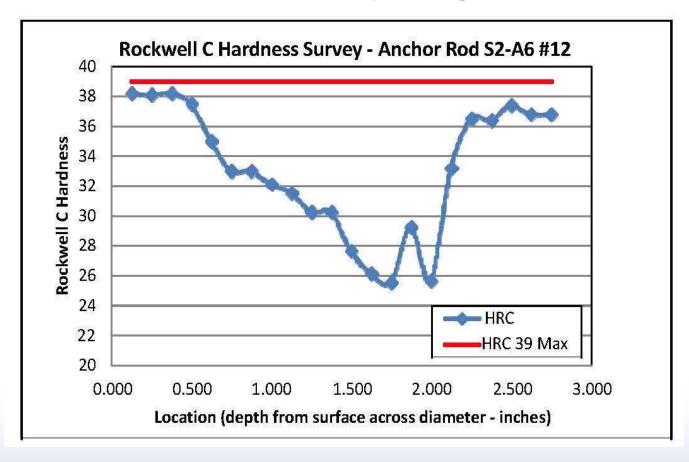


## **Bearings and Shear Keys on Pier E2**





## 2008 Rods Failed Due to Hydrogen Embrittlement



• Rods exhibited a material susceptibility to hydrogen embrittlement with a heterogenous structure and high surface hardness.



# TBPOC Investigation of High Strength Steel Rods

- Conducted four half-day workshops and held
   25+ other meetings or conference calls
- Reviewed over 5,000 pages of material
- Consulted with industry experts, Seismic Peer Review Panel, and FHWA team
- Briefed BATA and Bay Area State Legislators on multiple occasions



# **SAS** Responsible Parties

- Caltrans is the Owner/Operator.
- TY Lin International/Moffatt & Nichol Design Joint Venture is the Engineer of Record.
- American Bridge/Fluor Joint Venture is the Contractor for the SAS Superstructure.

## Findings – Owner, Designer, Contractor

- Per the joint metallurgical report, 2008 rods had "...higher than normal susceptibility of the steel to hydrogen embrittlement," but complied with specifications selected by the designer and owner of project
- Embedded rod design did not adequately address drainage, while contractor did not adequately provide on-site protection of 2008 rods from the environment during construction

# Findings – Owner & Designer

- Failed to consider different uses and tension levels for high-strength rods on SAS
- Did not adequately evaluate alternative rod materials and procurement methods (i.e., sole sourcing)
- Did not account for combined effect of rod type selection and corrosion protection methods

# Findings – Owner & Designer (con't)

- Failed to adequately consider corrosion protection alternatives to hot-dip galvanizing
- Relied too heavily on general ASTM guidance for contract specifications versus project-specific special provisions for steel hardness, toughness, and material testing

# Findings – Owner & Contractor

 Should have provided better coordination between the design and construction teams to ensure adequate material testing for hydrogen embrittlement.

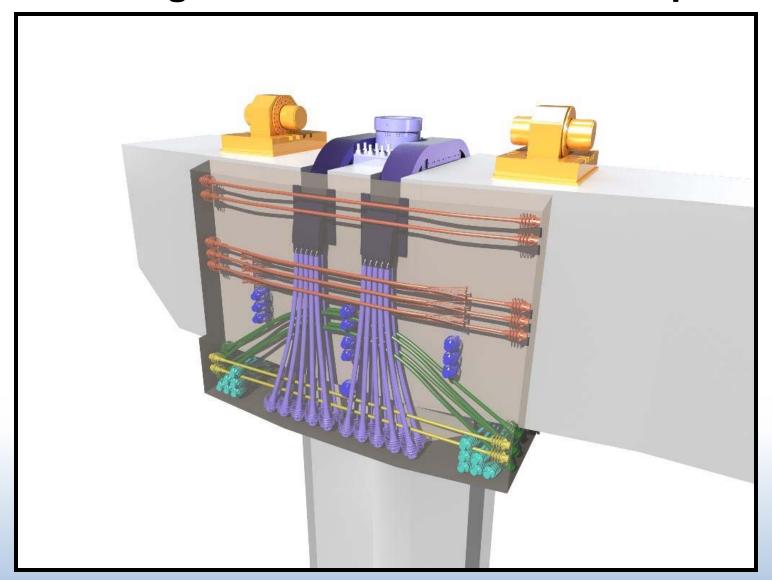
# Findings – Owner

 Failed to retain complete records in an easily retrievable format for new East Span contracts

# **Looking Forward**



## Rendering of Selected Steel Saddle Option



## **Status of Retrofit**

- Fabrication on-going at XKT Engineering on Mare Island in Vallejo, CA and Steward Machine Co. in Birmingham, AL.
- Field preparation on-going with machining of shear key bases and concrete preparation of Pier E2 cap.





# Retrofit Schedule & Bridge Opening

- Contractor forecasts shear key retrofit completion by December 10, 2013
- TBPOC will select bridge opening date based on retrofit completion, weather windows, and traffic impact
- Bridge opening may not coincide with Monday holiday weekend and will involve shorter advance notice

#### All Other Rods Performing As Designed Since Tensioning

Item #	Fabricator	End of Fabrication	Tension or Loading Complete	# of Rods Installed	# of Fractured Rods After Tensioning	Days Under Tension Through July 1, 2013
1	Dyson	Sep 2008	Mar 2013	96	32	Rods began failing after 3 days of tensioning
2	Dyson	Mar 2010	Apr 2013	192	0	91
3	Dyson	Mar 2010	Sep 2012	320	0	295
4	Dyson	Mar 2010	Sep 2012	224	0	292
5	Dyson	Aug 2009	Jun 2009	96	0	1,429
6	Dyson	Dec 2009	Jan 2010	336	0	1,245
7	Dyson	Nov 2011	Sep 2012	274	0	278
8	Dyson	Jul 2010	Jul 2012	25	0	351
9	Dyson	Jan 2011	Jul 2012	108	0	351
10	Dyson	Jan 2011	Mar 2013	90	0	97
11	Dyson	Oct 2011	Jul 2012	4	0	334
12	Vulcan Threaded Products	Feb 2007	Mar 2011	388	0	821
13	Vulcan Threaded Products	Feb 2007	Mar 2011	36	0	821
14	Dyson	Jun 2010	May 2010	32	0	1,125
15	Dyson	May 2010	Apr 2012	18	0	443
16	Dyson	Oct 2012	Feb 2013	24	0	142
17	Dyson	Jun 2009	In Design	43	0	-



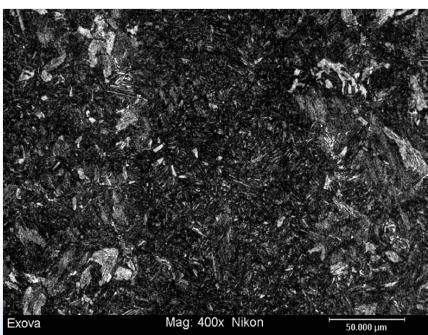
# **Improved Microstructure**

#### Failed 2008 Rod

#### **Other Rod**



Structure is not fully tempered martensite. The center region did not fully transformed into martensite



Essentially martensitic structure.



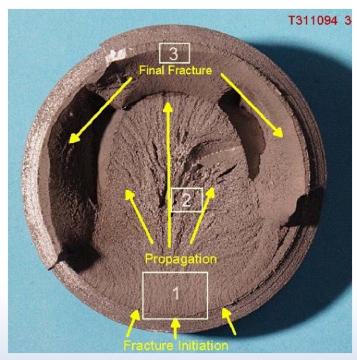
# **Improved Microstructure**

#### Failed 2008 Rod



**Brittle Failure in Field** 

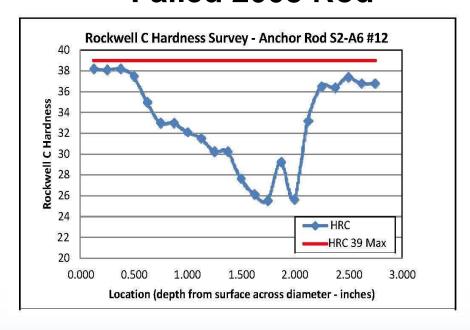
#### **Other Rod**



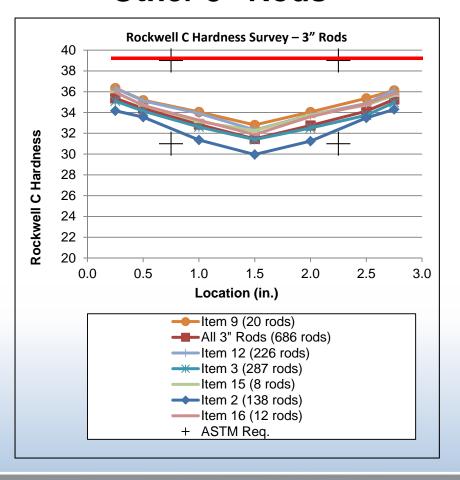
Ductile Failure in Lab
Test

## **Improved Hardness**

#### Failed 2008 Rod

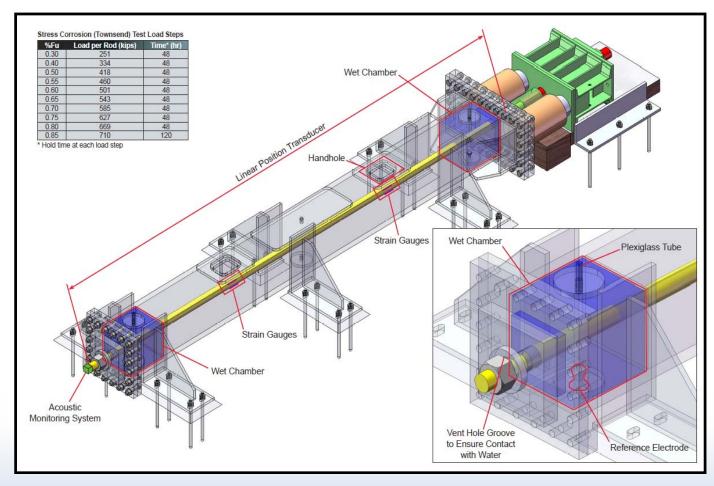


#### Other 3" Rods





## 3D Rendering of Stress Corrosion Test Platform

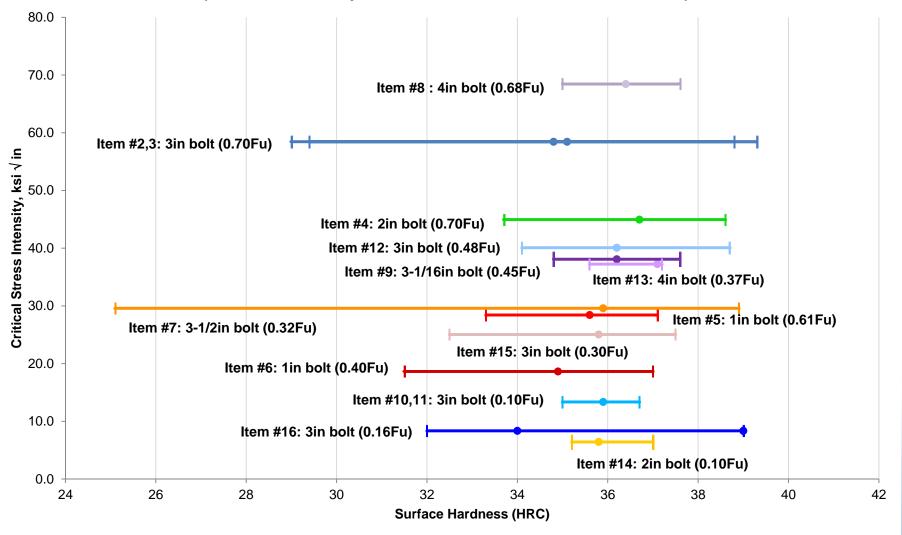


- Test platform being fabricated at Pier 7.
- First tests to begin the week of July 22, 2013



# Critical Stress Intensity vs. Surface Hardness Townsend Formulation

(Based on Rod by Rod Data from Test 1: June 21, 2013)





#### **Rod By Rod Resolution (Provisional)**

	Construction				
Location	Replace Before Opening (96)	Replace After Opening (740)	Reduce Tension (557)	Augment Dehumidification (274)	Accept and Monitor (639)
E2	<ol> <li>Shear Key Anchor Rods (bottom) (96)*</li> <li>replaced by steel saddle retrofit</li> </ol>	<ol> <li>Bearing &amp; Shear Key Anchor Rods (bottom) (192)</li> <li>Shear Key Rods (top) (320)</li> <li>Bearing Rods (top) (224)</li> </ol>			<ul><li>5. Bearing Assembly (96)</li><li>6. Bearing Retainer Ring Plate Assembly (336)</li></ul>
Anchorage				7. PWS Anchor Rods (274)	
Top of Tower		11. Outrigger Boom (4)	<ul><li>8. Saddle Tie Rods (25)</li><li>9. Saddle Turned Rods (108)</li></ul>		10. Saddle Grillage (90)
Bottom of Tower			12. Tower Anchor Rods (Type 1) (388) 13. Tower Anchor Rods (Type 2) (36)		
East Saddle					<ul><li>14. East Saddle Anchor Rods (32)</li><li>15. East Saddle Tie Rods (18)</li></ul>
East Cable					16. Cable Band Anchor Rod (24)
W2					17. Bikepath Anchor Rods – (43)

Note: Dehumidification is already in place for the Top of Tower, Bottom of Tower and Main Cable Anchorage.

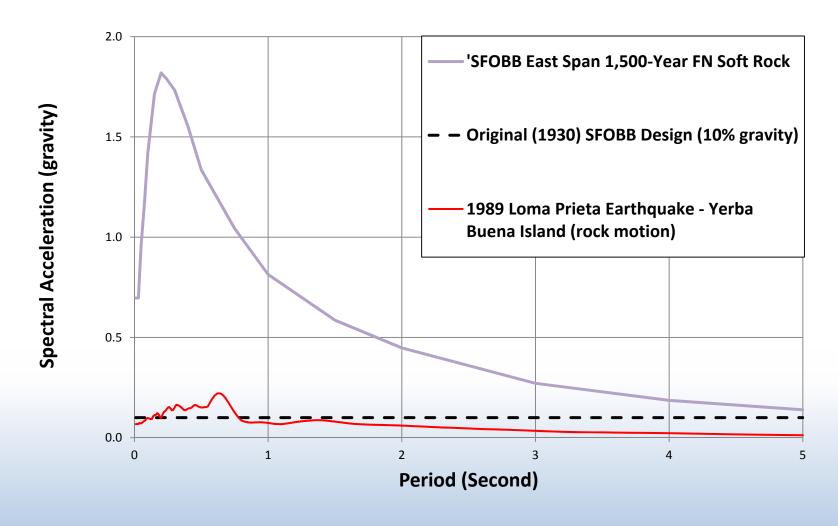


# New Bridge versus Old Bridge





### **Comparison of Ground Accelerations**



### **Bottom Line**

- It is safe to open the new East Span after replacing the capacity lost by the failed 2008 rods.
- The risk of near-term hydrogen embrittlement has passed.
- The potential for longer-term stress corrosion can be managed safely and effectively after SAS is placed into service.